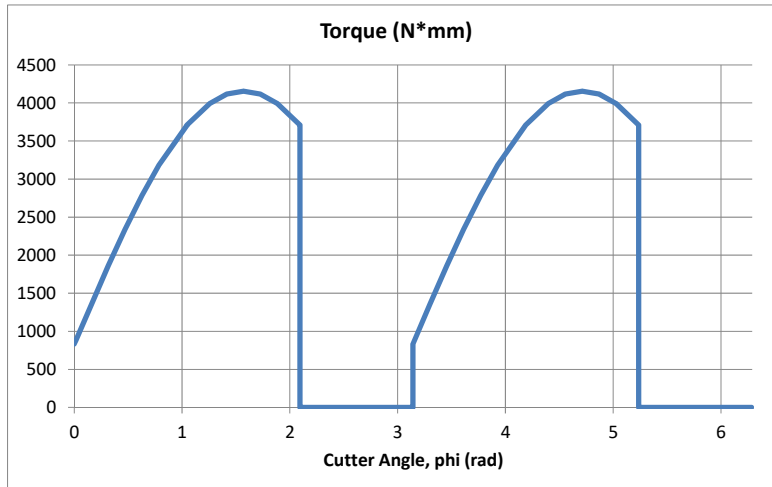


MSE 480/780 – Mid-Term Exam Solutions (Spring 2017)

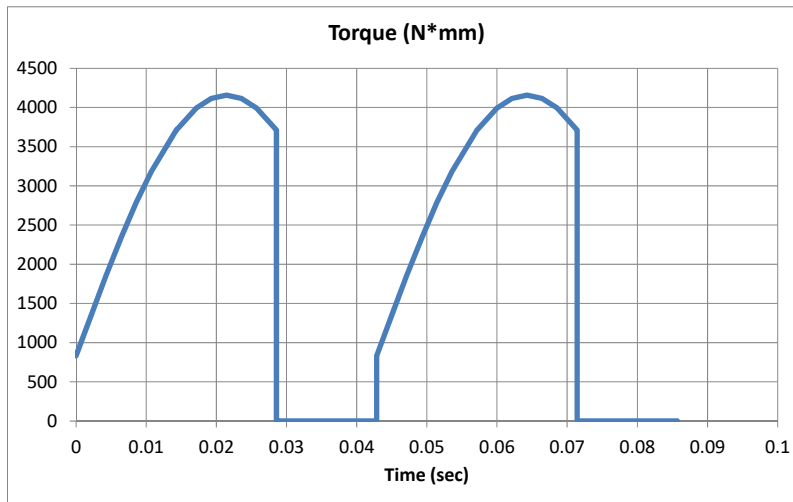
Problem 1 (20 Marks)

Part a (5 marks)

Plotting T_c versus cutter angle:



Alternatively plotting versus time:



Part b (5 marks)

- Max Cutting Torque, T_c : $RK_1as_t(\sin(\pi/2)+h^*/s_t) = \mathbf{4.156 \text{ N*m}}$
- Max Tangential Force, F_t : $K_1as_t(\sin(\pi/2)+h^*/s_t) = \mathbf{332.5 \text{ N}}$
- Max Thrust Force, F_{th} : $K_1as_t(r_1\sin(\pi/2)+r_2h^*/s_t) = \mathbf{212.8 \text{ N}}$
- Max Radial Force, F_r : $F_{th}\cos(\Psi) = \mathbf{150.5 \text{ N}}$
- Max Axial Force, F_z : $F_{th}\sin(\Psi) = \mathbf{150.5 \text{ N}}$

Part c (5 marks)

Power can be calculated as:

$$P = (\text{Torque}) * (\text{Spindle Speed})$$

$$= \Omega * R * K_1 * a * s * t * (\sin(\phi) + h^*/h_{eq})$$

Given 2/3 immersion and $h_{eq} \sim s \cdot t$:

$$\Rightarrow P_{max} \sim \Omega * R * K_1 * a * (s \cdot t + h^*)$$

e.g. calculated (max) power from part a

304.7 W

Maximum spindle power

400 W

$$\text{Maximum feed per tooth (st)}_{max} = P_{max} / (\Omega * R * K_1 * a) - h^*$$

$$(\text{st})_{max} = 0.055645003 \text{ mm}$$

Maximum feed per revolution ($s = 2 * st$)	0.111 mm
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*** Using P_{max} is conservative; also OK to calculate based on P_{avg} as follows

Integrating over 1/2 revolution (period of signal) with 2/3 immersion yields:

$$P_{avg} \sim (1/\pi) * \Omega * R * K_1 * a * (1 - \cos((2 * \pi)/3)) * s \cdot t + (2/3) * \Omega * R * K_1 * a * h^*$$

e.g. calculated (avg) power from part a

157.0 W

Letting $A =$

$$(1/\pi) * \Omega * R * K_1 * a * (1 - \cos((2 * \pi)/3)) = 2909.4$$

and letting $B =$

$$(2/3) * \Omega * R * K_1 * a * h^* = 40.6$$

$$\Rightarrow P_{avg} = A * s \cdot t + B$$

$$\text{Maximum feed per tooth (st)}_{max} = (P_{max} - B) / A$$

$$(\text{st})_{max} = 0.12352394 \text{ mm}$$

Maximum feed per revolution ($s = 2 * st$)	0.247 mm
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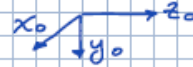
Problem 2 (20 Marks)

Part a (5 marks)

- LOOKING AT $A_{0,1}(\theta_1)$ IT CAN BE SEEN THAT JOINT #1 IS REVOLUTE.
- IT CAN ALSO BE SEEN THAT THE AXIS OF ACTUATION FOR JOINT #2 (z_1) IS ORIENTED AS SHOWN:

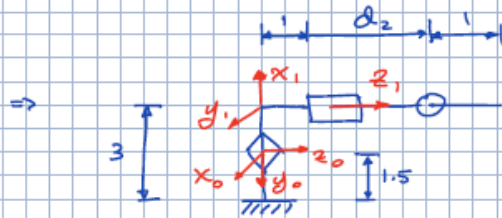


- THE ROTATION MATRIX $R_{0,1}$ SHOWS THAT z_0 IS PARALLEL WITH z_1 , SO FRAME F_0 IS ORIENTED AS FOLLOWS:



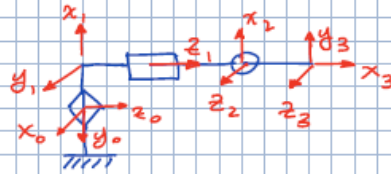
- WHEN $\theta_1 = 0$, THE DISPLACEMENT VECTOR

$$\vec{d}_{0,1}^0 = [0, -1.5, 0]^T \text{ AND } R_{0,1} = \begin{bmatrix} 0 & 1 & 0 \\ -1 & 0 & 0 \\ 0 & 0 & 1 \end{bmatrix}$$



Part b (10 marks)

• ADDING FRAMES TO THE REST OF THE MANIPULATOR, FOLLOWING THE DH CONVENTION AND REFERRING TO $A_{0i}(\theta_i)$ AS PROVIDED:



⇒

JOINT	a_i	α_i	d_i	θ_i
1	1.5	0	0	$\theta_1 - \pi/2$
2	0	$-\pi/2$	$1 + d_2$	0
3	1	0	0	$\theta_3 - \pi/2$

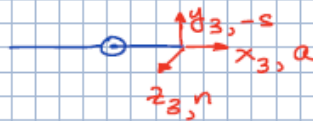
⇒

$$A_{12}(d_2) = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & -1 & 0 & 1 + d_2 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$A_{23}(\theta_3) = \begin{bmatrix} s\theta_3 & c\theta_3 & 0 & s\theta_3 \\ -c\theta_3 & s\theta_3 & 0 & -c\theta_3 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

Part c (5 marks)

BY INSPECTION:



$$A_{3E} = \begin{bmatrix} 0 & 0 & 1 & 0 \\ 0 & -1 & 0 & 0 \\ 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$